

## SKIN FRICTION COEFFICIENT AND NUSSELT NUMBER IN FLUID FLOW AND HEAT TRANSFER BETWEEN TWO VERTICAL PLATES-II

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### INTRODUCTION

I studied the problem of three-dimensional free convective heat transfer between two long vertical plates, moving in opposite directions with equal velocities. The cosinusoidal suction velocity as a function of spanwise component  $z$  is applied normal to the plate and temperature of the downward moving plate is taken spanwise cosinusoidal. The governing equations are solved using regular perturbation technique. The obtained solutions are functions of dimensionless parameters Grashof number, Prandtl number and cross-flow Reynolds number. The expressions for skin friction coefficient and the rate of heat transfer at both the plates are also obtained and numerical values are presented in the form of tables for various combination of these parameters.

### PROBLEM FORMULATION

The three-dimensional flow of a viscous incompressible fluid between two long vertical plates at a distance 'd' apart. The plates are moving in opposite directions with equal velocity  $U_0^*$ . Let  $x^*$  - axis be along the plate in vertical upward direction and  $y^*$  - axis normal to the plate. The  $x^*$  and  $z^*$  axis are in the plane of the plate at  $y^* = 0$ .

Consider the suction velocity at  $y^* = 0$  as

$$v^* = -V_0 \left(1 + \epsilon \cos \frac{\pi z^*}{l}\right) \dots\dots\dots (1)$$

and the temperature of the downward moving plate as

$$T^* = T_d + (T_s - T_d) \left(1 + \epsilon \cos \frac{\pi z^*}{l}\right) \dots\dots\dots (2)$$

where 'l' is wavelength,  $T_d$  the constant temperature of the plate at  $y^* = d$  and  $T_s$  is some constant

temperature. The plates are large compared to distance between them. All physical variables are assumed to be independent of  $x^*$ . If  $(u^*, v^*, w^*)$  be the velocity components in  $x^*, y^*, z^*$  direction respectively, then Navier-Stokes equations and energy equation are

$$\frac{\partial v^*}{\partial y^*} + \frac{\partial w^*}{\partial z^*} = 0 \dots\dots\dots (3)$$

$$v^* \frac{\partial u^*}{\partial y^*} + w^* \frac{\partial u^*}{\partial z^*} = \nu \left[ \frac{\partial^2 u^*}{\partial y^{*2}} + \frac{\partial^2 u^*}{\partial z^{*2}} \right] + g \beta (T^* - T_d) \dots\dots\dots (4)$$

$$v^* \frac{\partial v^*}{\partial y^*} + w^* \frac{\partial v^*}{\partial z^*} = \nu \left[ \frac{\partial^2 v^*}{\partial y^{*2}} + \frac{\partial^2 v^*}{\partial z^{*2}} \right] \dots\dots\dots (5)$$

$$v^* \frac{\partial w^*}{\partial y^*} + w^* \frac{\partial w^*}{\partial z^*} = \nu \left[ \frac{\partial^2 w^*}{\partial y^{*2}} + \frac{\partial^2 w^*}{\partial z^{*2}} \right] \dots\dots\dots (6)$$

$$v^* \frac{\partial T^*}{\partial y^*} + w^* \frac{\partial T^*}{\partial z^*} = \frac{k}{\rho C_p} \left[ \frac{\partial^2 T^*}{\partial y^{*2}} + \frac{\partial^2 T^*}{\partial z^{*2}} \right] \dots\dots\dots (7)$$

where  $k$  is thermal conductivity and  $\beta$  is volumetric coefficient of thermal expansion of the fluid.

The boundary conditions are:

$$y^* = 0, u^* = -U_0^*, v^* = -V_0 \left(1 + \epsilon \cos \frac{\pi z^*}{l}\right), w^* = 0,$$

$$T^* = T_d + (T_s - T_d) \left(1 + \epsilon \cos \frac{\pi z^*}{l}\right)$$

$$y^* = d, u^* = U_0^*, v^* = -V_0, w^* = 0, T^* = T_d \dots\dots (8)$$

Now let us introduce following dimensionless variables

$$x = \frac{x^*}{d}, y = \frac{y^*}{d}, z = \frac{z^*}{d}, u = \frac{u^* d}{\nu}, v = \frac{v^* d}{\nu}, w = \frac{w^* d}{\nu},$$

$$U_0 = \frac{U_0^* d}{v}, \theta = \left( \frac{T^* - T_d}{T_s - T_d} \right) \dots\dots\dots(9)$$

The corresponding boundary conditions are :

$$y = 0, \begin{cases} u = -U_0 v = -R(1 + \epsilon \cos \pi \lambda z) \\ w = 0, \theta = 1 + \epsilon \cos \pi \lambda z \end{cases}$$

$$y = 1, u = U_0, v = -R, w = 0, \theta = 0 \dots\dots(10)$$

And the involved dimensionless parameters are :

$$R = \frac{V_0 d}{v} \text{ (cross flow Reynold number)}$$

$$Pr = \frac{\mu C_p}{k} \text{ (Prandtl number)} \lambda = d/l$$

$$G = g \frac{\beta d^3 (T_s - T_d)}{v^2} \text{ (Grashof number)} \dots\dots\dots(11)$$

### SKIN-FRICTION COEFFICIENT AND NUSSELT NUMBER

The skin-friction coefficient at both the plates are given by

$$C_{fx} = \frac{\tau_x}{\frac{\rho v^2}{2}} = real \left( \frac{\partial u}{\partial y} \right)_{y=0, y=1} \dots\dots\dots (12)$$

$$C_{fx} \Big|_{y=0, y=1} = \left[ -C_7 R e^{-Ry} - \frac{C_3 G e^{-RPr y}}{R(1-Pr)} \right] + \epsilon \cos \pi \lambda z$$

$$\begin{aligned} & [m_1 C_{13} e^{m_1 y} + m_2 C_{14} e^{m_2 y} - \\ & G \{ D_5 m_3 e^{m_3 y} + D_6 m_4 e^{m_4 y} \\ & + D_7 R Pr e^{-RPr y} + D_8 (m_1 - R Pr) e^{(m_1 - R Pr) y} \\ & + D_9 (m_2 - R Pr) e^{(m_2 - R Pr) y} \} - \pi \lambda \{ -R D_{10} e^{-Ry} \\ & - D_{11} (m_1 - R) e^{(m_1 - R) y} - D_{12} (m_2 - R) e^{(m_2 - R) y} \\ & - D_{13} R Pr e^{-R Pr} - D_{14} e^{(m_1 - R Pr) y} \times (m_1 - R Pr) \\ & - D_{15} (m_2 - R Pr) e^{(m_2 - R Pr) y} \} \dots\dots\dots(13) \end{aligned}$$

The dimensionless coefficient of heat transfer i.e. Nusselt number are given by

$$Nu = - \frac{q}{\rho V_0 C_p (T_s - T_d)} = - \left( \frac{\partial \theta}{\partial y} \right)_{y=0, y=1} \dots\dots(14)$$

$$\begin{aligned} Nu \Big|_{y=0, y=1} &= - [ -R Pr C_3 e^{-RPr y} + \epsilon \cos \pi \lambda z \\ & \{ C_{11} m_3 e^{m_3 y} + m_4 C_{12} e^{m_4 y} - \\ & C_3 R \pi \lambda Pr^2 (-D_1 R Pr e^{-RPr y} \\ & + D_2 (m_1 - R Pr) e^{(m_1 - R Pr) y} + D_3 (m_2 - \\ & R Pr) e^{(m_2 - R Pr) y} \} ] \dots\dots(15) \end{aligned}$$

The skin-friction coefficient and Nusselt number at both the plates  $y = 0$  and  $y = 1$  for various combination of parameters (Table-I) are given in Table II, III, IV, V.

TABLE -I: Various Combinations Of Parameters

Case	R	Pr	G	$\lambda$	$\epsilon$
I	-2	0.7	5	0.1	0.1
II	2	0.7	5	0.1	0.1
III	20	0.7	5	0.1	0.1
IV	40	0.7	5	0.1	0.1
V	2	7	5	0.1	0.1
VI	2	7	5	0.3	0.1
VII	2	0.7	10	0.1	0.1
VIII	2	0.7	15	0.1	0.1
IX	2	0.7	5	0.1	0.3

**TABLE-II:Skin friction coefficient  $C_{fx}$  vs  $\pi \lambda z$  Case at the plate  $y = 0$**

Case/ $\pi \lambda z$	I	II	III	IV	V	VI	VII	VIII	IX
$\pi \lambda z = 0$	- 68.3008 5	28.1908	29.5781 3	33.5	0.52856	0.7406	55.90772	83.6233	78.232 67
$\pi \lambda z = \frac{\pi}{4}$	- 48.0511 2	20.6843 3	22	25.625	0.61312 49	0.7615	40.89807	61.1110 9	55.713 88
$\pi \lambda z = \frac{\pi}{2}$	.- 8016782	3.16974 8	4.35714 3	8.1785 2	0.8104	0.8104	5.87689	8.58403 8	3.1697 48
$\pi \lambda z = \frac{3\pi}{4}$	46.4477 6	- 14.3448 5	- 13.2812 5	-9.25	1.0077	0.85929	- 29.14429	-43.943	49.373 78
$\pi \lambda z = \pi$	66.6974 8	-21.8512	- 20.8593 8	-17	1.0923	0.88023 18	- 44.15381	- 66.4553 3	- 71.893 07
$\pi \lambda z = \frac{5\pi}{4}$	46.4477 6	- 14.3448 5	- 13.2812 5	-9.25	1.0077	0.85929	- 29.14429	-43.943	49.373 78

**Table – III: Skin friction coefficient  $C_{fx}$  vs  $\pi \lambda z$  Case at the plate  $y = 1$**

Case/ $\pi \lambda z$	I	II	III	IV	V	VI	VII	VIII	IX
$\pi \lambda z = 0$	216.91 41	- 8.8133 9	$-5.2 \times 10^{-5}$	$3.097548 \times 10^{-5}$	$6.086136 \times 10^{-2}$	$5.897142 \times 10^{-2}$	- 17.687 26	- 26.561 04	- 24.836 7
$\pi \lambda z = \frac{\pi}{4}$	152.79 06	- 6.4098 67	$-3.6 \times 10^{-5}$	$2.168284 \times 10^{-5}$	.0585892	$5.72672 \times 10^{-2}$	- 12.880 88	- 19.351 81	- 17.626 22
$\pi \lambda z = \frac{\pi}{2}$	3.1697 49	- .80167 85	- $6.8224 \times 10^{-5}$	$-2.8880633 \times 10^{-13}$	$5.32908 \times 10^{-2}$	$5.329088 \times 10^{-2}$	- 1.6659 64	- 2.5302 249	- .80167 85
$\pi \lambda z = \frac{3\pi}{4}$	- 146.45 1	4.8065	$3.54341 \times 10^{-5}$	$-2.168284 \times 10^{-5}$	$4.799199 \times 10^{-2}$	0.0493145	9.5489 35	14.291 32	16.022 89
$\pi \lambda z = \pi$	- 210.57 45	7.2099 76	$5.091256 \times 10^{-5}$	$3.097548 \times 10^{-5}$	$4.572058 \times 10^{-2}$	$4.761033 \times 10^{-2}$	14.355 32	21.500 55	23.233 37
$\pi \lambda z = \frac{5\pi}{4}$	- 146.45 1	4.8065 04	$3.543415 \times 10^{-5}$	$-2.168284 \times 10^{-5}$	$4.799199 \times 10^{-2}$	.0493145	9.5489 35	14.291 32	16.022 89

**Table – IV; Nusselt number vs  $\pi \lambda z$  Case at the plate  $y = 0$**

Case/ $\pi \lambda z$	I	II	III	IV	V	VI	VII	VIII	IX
$\pi \lambda z = 0$	.473694 3	2.13030 6	16.7250 1	33.6	16.775	16.7796	2.130306	2.130306	2.67444 6
$\pi \lambda z = \frac{\pi}{4}$	.469056 6	2.04868 4	15.9075 1	31.9 2	15.9425 1	15.9457 3	2.048684	2.048684	2.42958 3
$\pi \lambda z = \frac{\pi}{2}$	.458235 2	1.85823 5	14.0000 1	28.	14.0000 1	14.0000 1	1.858235	1.858235	1.85235
$\pi \lambda z = \frac{3\pi}{4}$	.447413 9	1.66778 6	12.0925 1	24.0 8	12.0575 1	12.0543	1.667786 4	1.667786 4	1.28688 8
$\pi \lambda z = \pi$	.442776 2	1.58616 5	11.2750 1	22.4	11.2250 1	11.2204 2	1.586165	1.586165	1.04202 4
$\pi \lambda z = \frac{5\pi}{4}$	.447413 9	1.66778 6	12.0925 1	24.0 8	12.0575 1	12.0543	1.667786 4	1.667786	1.28688 8

**Table – V: Nusselt number vs  $\pi \lambda z$  / Case at the plate  $y = 1$**

Case/ $\pi \lambda z$	I	II	III	IV	V	VI	VII	VIII	IX
$\pi \lambda z = 0$	2.093 573	.4843 903	5.919363 $\times 10^{-6}$	1.89801 $\times 10^{-12}$	6.712105 $\times 10^{-6}$	4.00475 $\times 10^{-6}$	.48439 03	.4843 903	0.5367 005
$\pi \lambda z = \frac{\pi}{4}$	2.022 972	.4765 438	7.635976 $\times 10^{-6}$	7.13699 $\times 10^{-12}$	8.190896 $\times 10^{-6}$	0.295748 $\times 10^{-6}$	.47654 38	.4765 438	0.5131 609
$\pi \lambda z = \frac{\pi}{2}$	1.858 235	.4582 352	1.164141 $\times 10^{-5}$	1.936031 $\times 10^{-11}$	1.64141 $\times 10^{-5}$	1.164141 $\times 10^{-5}$	.45823 52	.4582 352	0.4582 352
$\pi \lambda z = \frac{3\pi}{4}$	1.693 409	.4399 266	1.564684 $\times 10^{-5}$	3.158392 $\times 10^{-11}$	1.509192 $\times 10^{-5}$	1.698707 $\times 10^{-5}$	.43992 66	.4399 266	0.4033 095
$\pi \lambda z = \pi$	1.622 897	.4320 801	1.736346 $\times 10^{-5}$	3.682261 $\times 10^{-11}$	1.657071 $\times 10^{-5}$	1.927807 $\times 10^{-5}$	.43208 01	0.432 0801	0.3797 699
$\pi \lambda z = \frac{5\pi}{4}$	1.693 409	.4399 266	1.564684 $\times 10^{-5}$	3.158392 $\times 10^{-11}$	1.509192 $\times 10^{-5}$	1.698707 $\times 10^{-5}$	.43992 66	.4399 266	0.4033 095

## RESULTS

The skin-friction coefficient and rate of heat transfer i.e. Nusselt number at both the plates  $y = 0$  and  $y = 1$  for various combination of parameters Table I and given in Table II, III, IV and V.

The coefficient of skin friction  $C_{fx}$  in the  $x$ -direction at  $y = 0$  increases with the increase of Reynolds number  $R$ , decrease of Prandtl number  $Pr$  and increase of  $\lambda$ . It also increases with the increase of Grashof number  $G$  and parameter  $\epsilon$ , Table II. The coefficient of skin friction at  $y = 1$  decreases with the increase of Reynold number  $R$ , decrease of Prandtl

number  $Pr$  and increase of  $\lambda$ .  $C_{fx}$  also decrease with the increase of Grashof number  $G$  and parameter  $\epsilon$ , Table III.

The rate of heat transfer i.e. Nusselt number  $Nu$  from the plate at  $y = 0$  increases with the increase of Reynold number  $R$ , an increase of Prandtl number and parameter  $\epsilon$  see Table IV. The Nusselt number  $Nu$  from the plate at  $y = 1$  decreases with the increase of  $R$ ,  $Pr$ ,  $\epsilon$ , see Table V. There is no

effect of Grashof number  $G$  on rate of heat transfer at both the plates situated at  $y = 0$  and  $y = 1$ .

## REFERENCES

**Bansal 2013: - Fluid flow and heat transfer between two vertical plates moving in opposite direction international research journal of science engineering and technology, RJSET vol 3 issue 1. And references therein.**

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